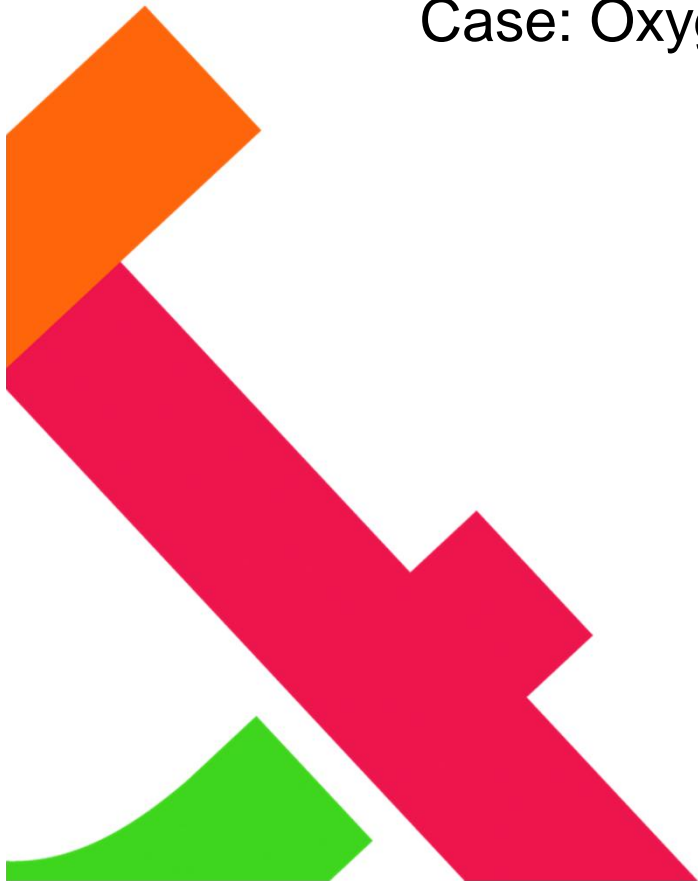


# Modelling of radiative heat transfer in a CFB furnace by correlation based zone method

Case: Oxygen fired combustion

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# Introduction

## Background

- A semi-empirical three-dimensional model for simulating a CFB furnace has been developed earlier (CFB3D).
  - Long distance radiation not considered.
- A radiative heat transfer model based on the zone method has been developed and applied for non-CFB conditions (e.g. pulverized combustion, backpass).

## Need

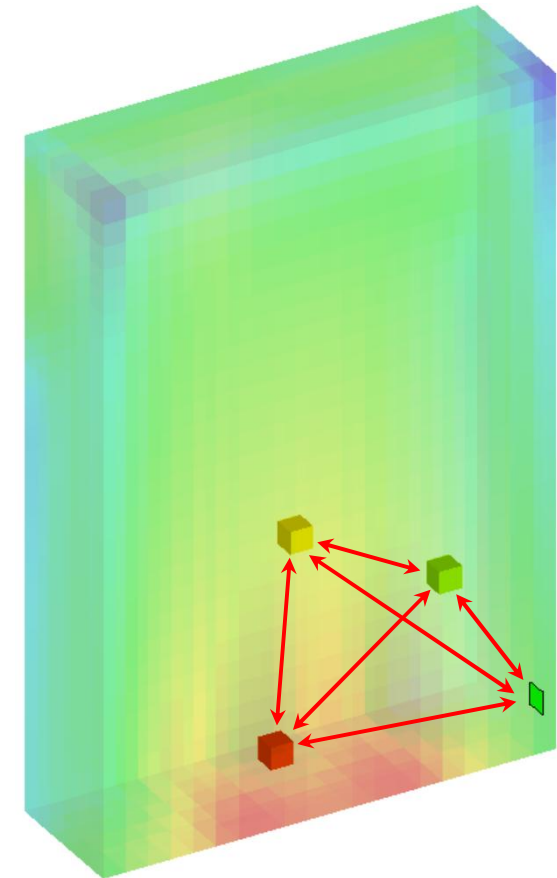
- In oxygen-fired CFB conditions, the proportion of radiative gases ( $\text{CO}_2$ ,  $\text{H}_2\text{O}$ ) is high => effect on the radiative heat transfer.
- The role of the radiative heat transfer is high in the upper dilute section of a CFB furnace and especially in low load conditions => long distance radiation to be considered.

## Solution

- The purpose of this work is to combine the radiative heat transfer model with the steady-state process model for circulating fluidized bed furnaces.
- The object of study is a large oxygen-fired CFB.
- The following presentation describes the method and initial model results.

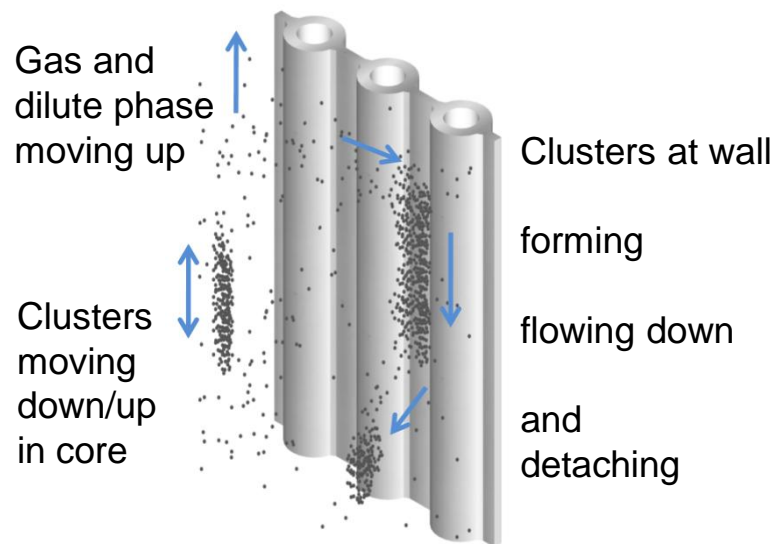
# Radiation model: zone method

- Principle is old (Hottel and Sarofim, Radiative Transfer, 1967).
- Calculation domain divided to volume zones and surface zones.
- Exchange factors determined between different zones.
- Coefficients for absorption, scattering, and emission defined for each cell and face.
  - In this implementation, weighted sum of gray gas model for gases was used.
  - Effect of particles added -> usually dominating.
- Radiative energy balances defined between each zones and solved.
  - ⇒ Radiative source terms in cells ( $\text{W}/\text{m}^3$ )
  - ⇒ Radiative heat flux at faces ( $\text{W}/\text{m}^2$ )
- Limitations of the current model:
  - Rectangular domains.
  - No internal heat exchanger surfaces.
  - Limited mesh size.

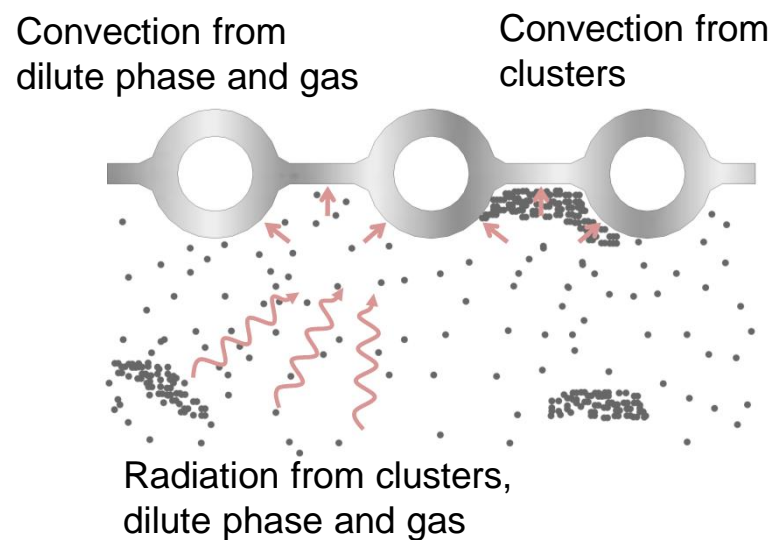


# Heat flux to CFB walls: principles

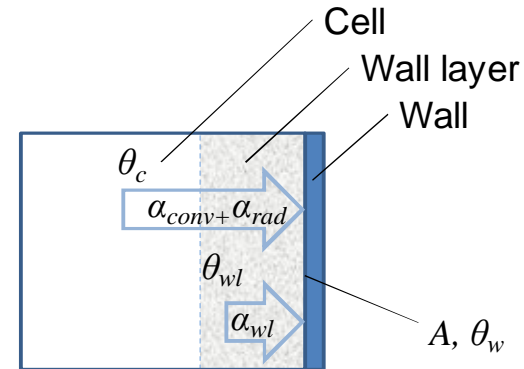
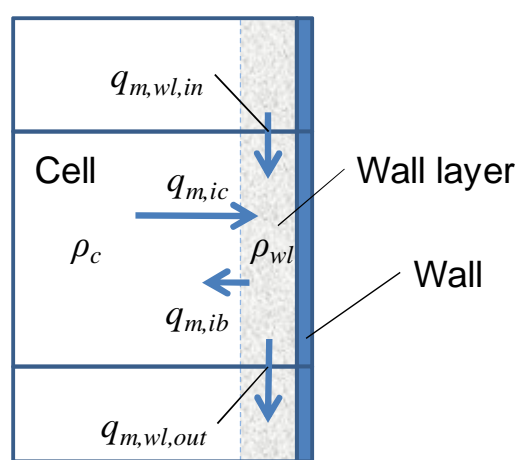
Fluid dynamics



Main heat flow modes



# Modeled heat flux modes in CFB3D



$$q''_{tot} = (\alpha_{conv} + \alpha_{rad})(\theta_c - \theta_w) + \alpha_{wl}(\theta_{wl} - \theta_w)$$

- Modeled heat transfer modes in CFB3D
  - Wall layer = convective heat transfer from wall layer to wall
  - Cell convective = convective heat transfer from cell to wall
  - Radiative = radiative heat transfer from cell to wall

$$\Rightarrow q''_{tot} = (\alpha_{conv} + \alpha_{rad})(\theta_c - \theta_w) + \alpha_{wl}(\theta_{wl} - \theta_w)$$

- When the radiation model is applied, the radiative heat flux is defined by the radiation model:

$$\Rightarrow q''_{tot} = \alpha_{conv}(\theta_c - \theta_w) + \alpha_{wl}(\theta_{wl} - \theta_w) + q''_{rad}$$

# Radiative source term

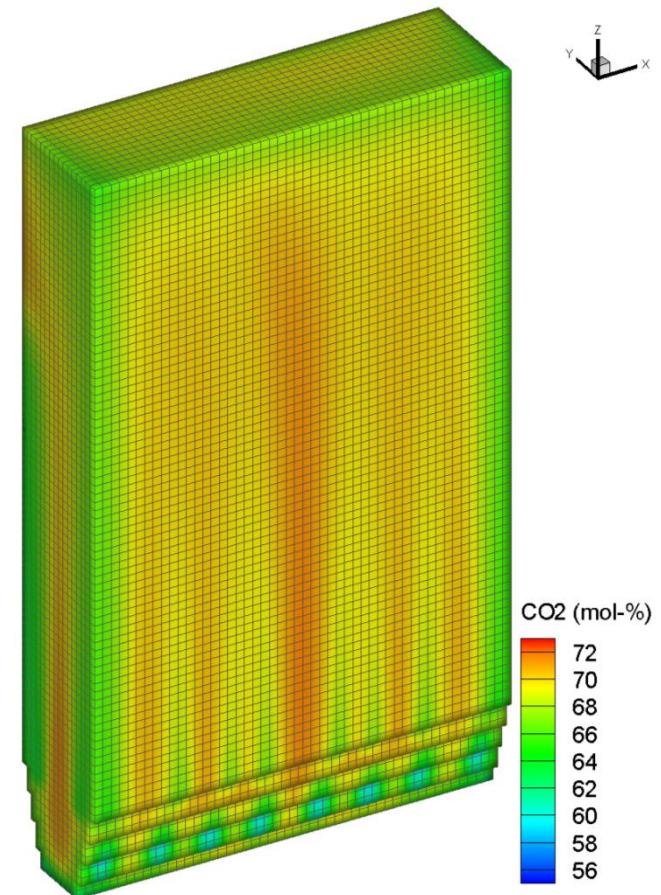
- The radiative source term is directly applied in the CFB3D-code as an extra heat source in the energy equation (see below).
- The radiation model (i.e. radiative source term) affects the mixing of energy inside the model domain.

Energy equation

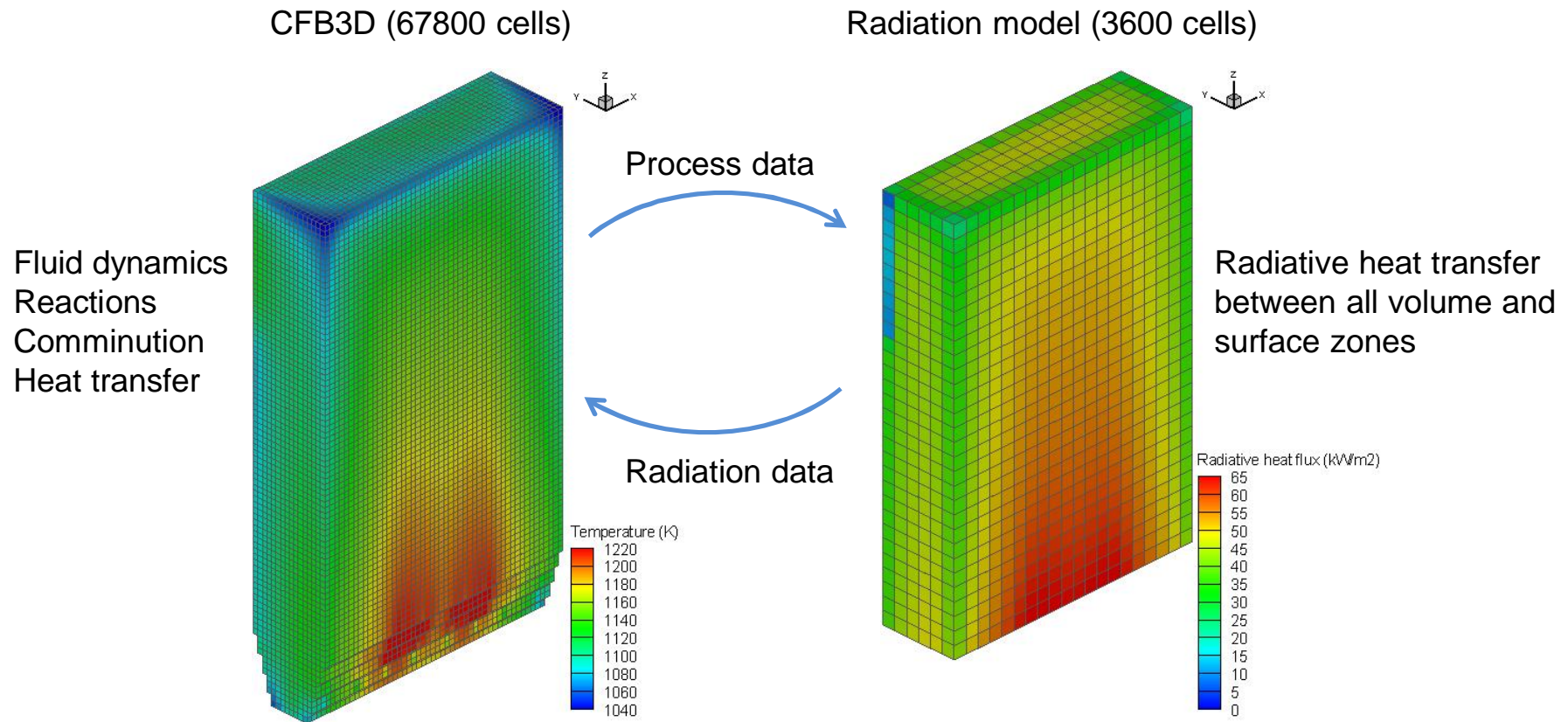
$$\begin{aligned}
 & \oint_A \varepsilon_g \rho_g c_{pg} T_c \mathbf{v}_g \cdot d\mathbf{A} + \oint_A \varepsilon_s \rho_s c_{ps} T_c \mathbf{v}_s \cdot d\mathbf{A} && \leftarrow \text{Convection of gas and solids} \\
 & - \oint_A \varepsilon_g \rho_g D_g c_{pg} \nabla T_c \cdot d\mathbf{A} - \oint_A \varepsilon_s \rho_s D_s c_{ps} \nabla T_c \cdot d\mathbf{A} && \leftarrow \text{Dispersion/diffusion of gas and solids} \\
 & = \int_V (\phi_g''' c_{pg} T_g + \phi_s''' c_{ps} T_s + \varphi''' + \underbrace{\varphi_{rad}'''}_{\text{Radiative source term}}) dV && \leftarrow \text{Sensible enthalpies of gas and solid feeds} \\
 & + \int_V \left( \sum_{rt} \frac{\partial m_{rt}'''}{\partial t} \frac{H_{0,rt}}{M_{rt}} - \sum_{pt} \frac{\partial m_{pt}'''}{\partial t} \frac{H_{0,pt}}{M_{pt}} \right) dV && \leftarrow \text{Additional volumetric heat sources} \\
 & - \oint_A \alpha_c (T_c - T_w) \cdot d\mathbf{A} && \leftarrow \text{Reaction enthalpies} \\
 & && \leftarrow \text{Heat transfer from cell to wall}
 \end{aligned}$$

# Calculation case: oxygen fired CFB

- Initial design of Compostilla (OXY-CFB-300).
  - Furnace size 25.2 m x 7.6 m x 44.0 m
  - 100% load point, thermal power  $\approx$  700 MW.
  - Inlet  $O_2 = 23.5$  %-vol.
  - Flue gas recycle ratio 69%.
- Flue gas composition:  
3%  $O_2$ , 70%  $CO_2$ , 21%  $H_2O$ , 6%  $N_2+Ar+other$
- The initial design did not have internal heat exchanger surfaces  
=> suitable for simplified radiation model.

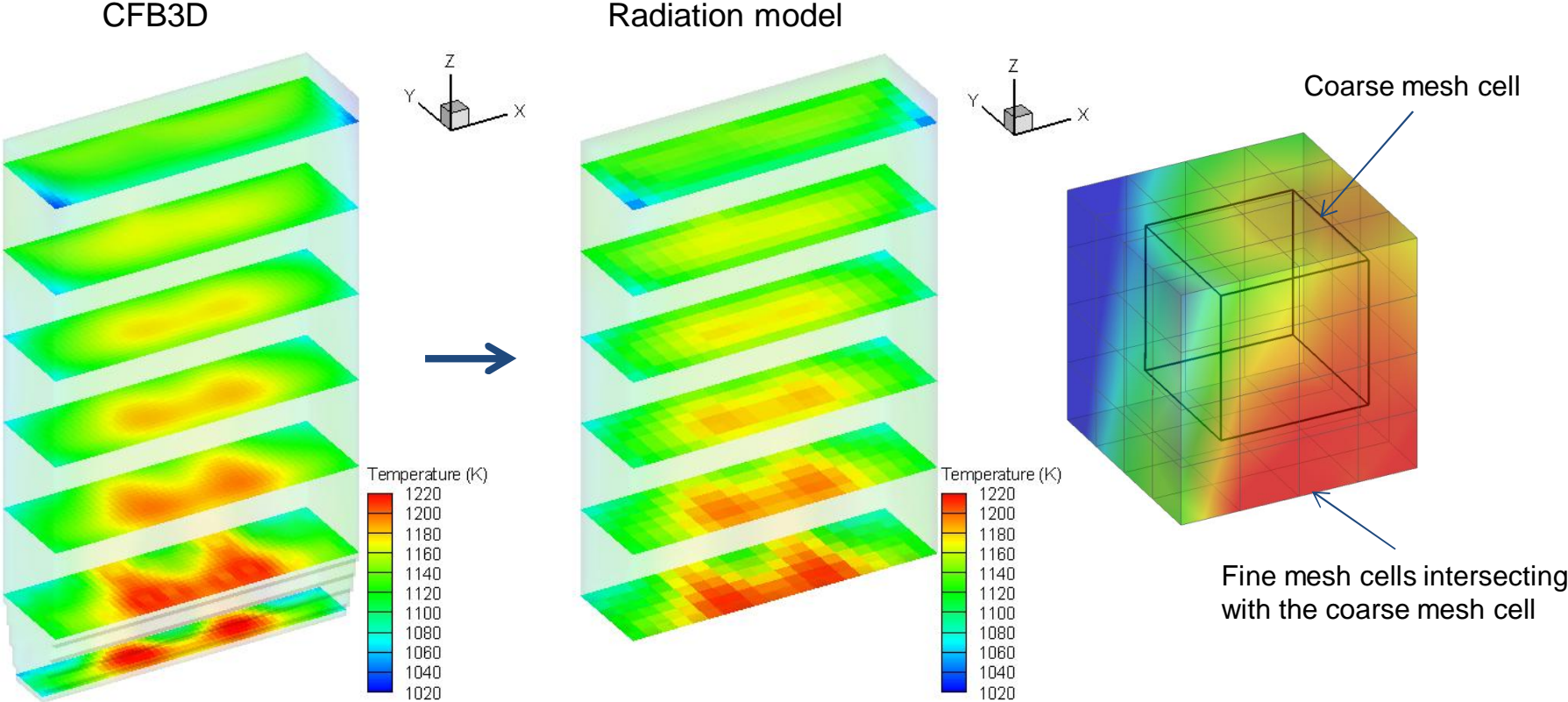


# Modelling concept

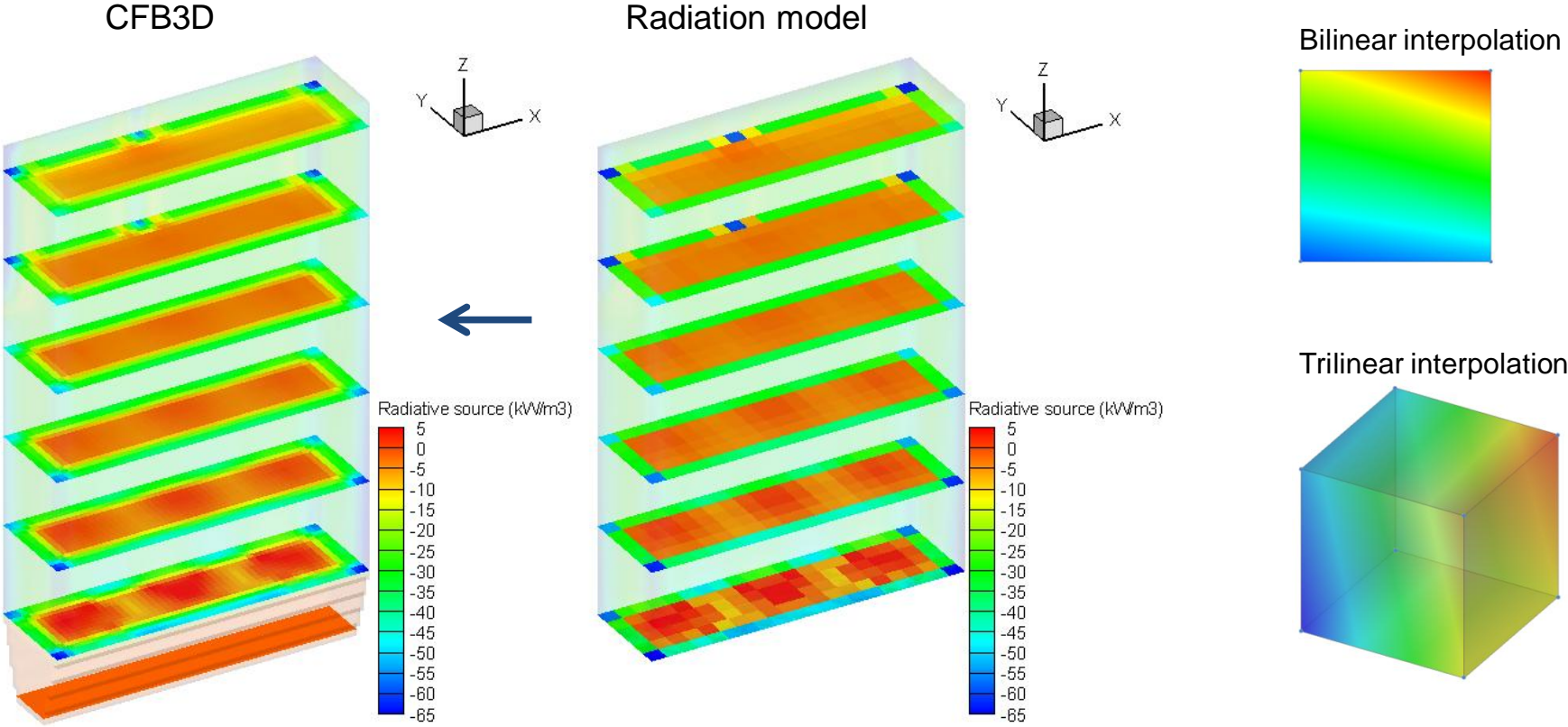




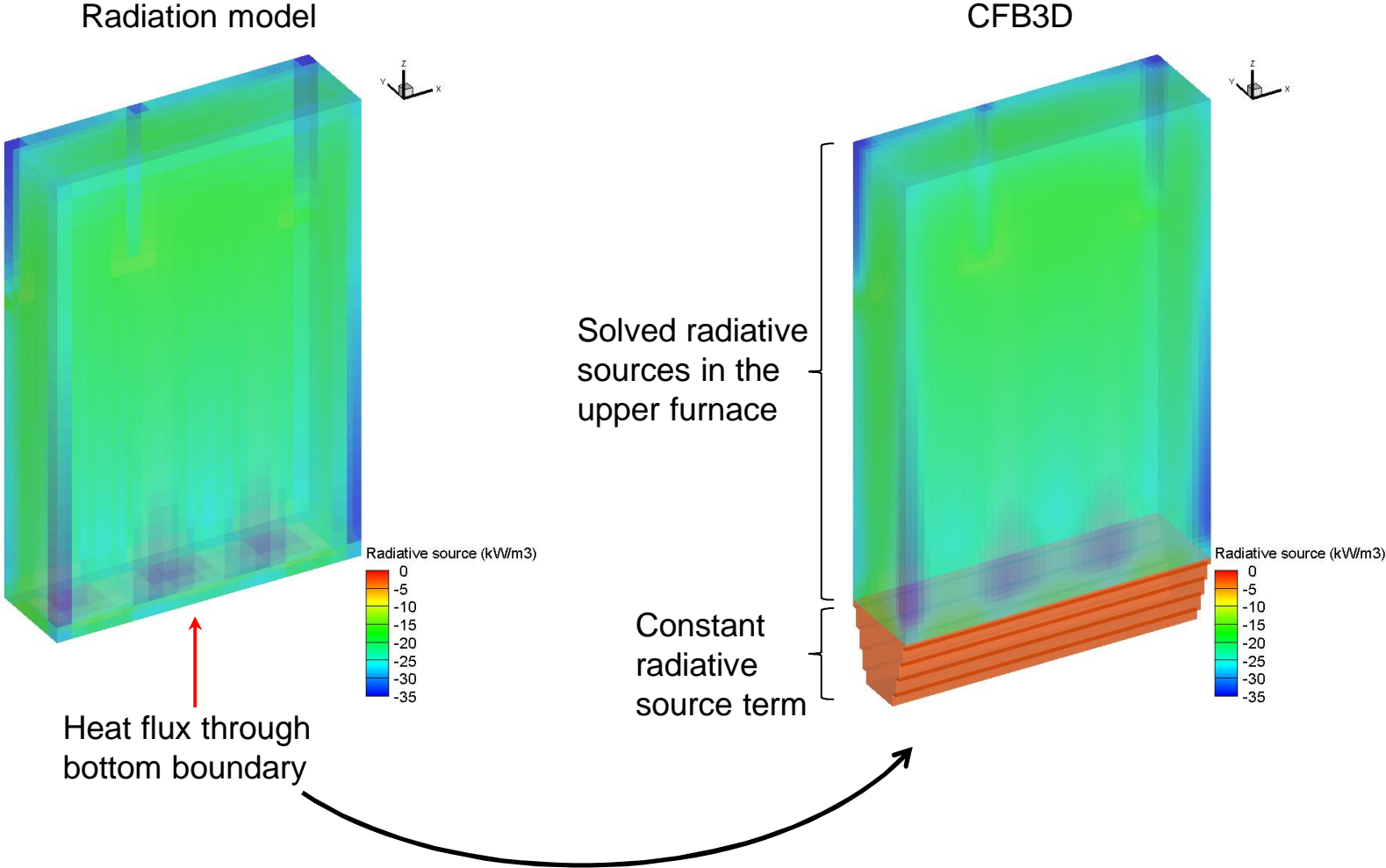
# Example of data exchange: temperature



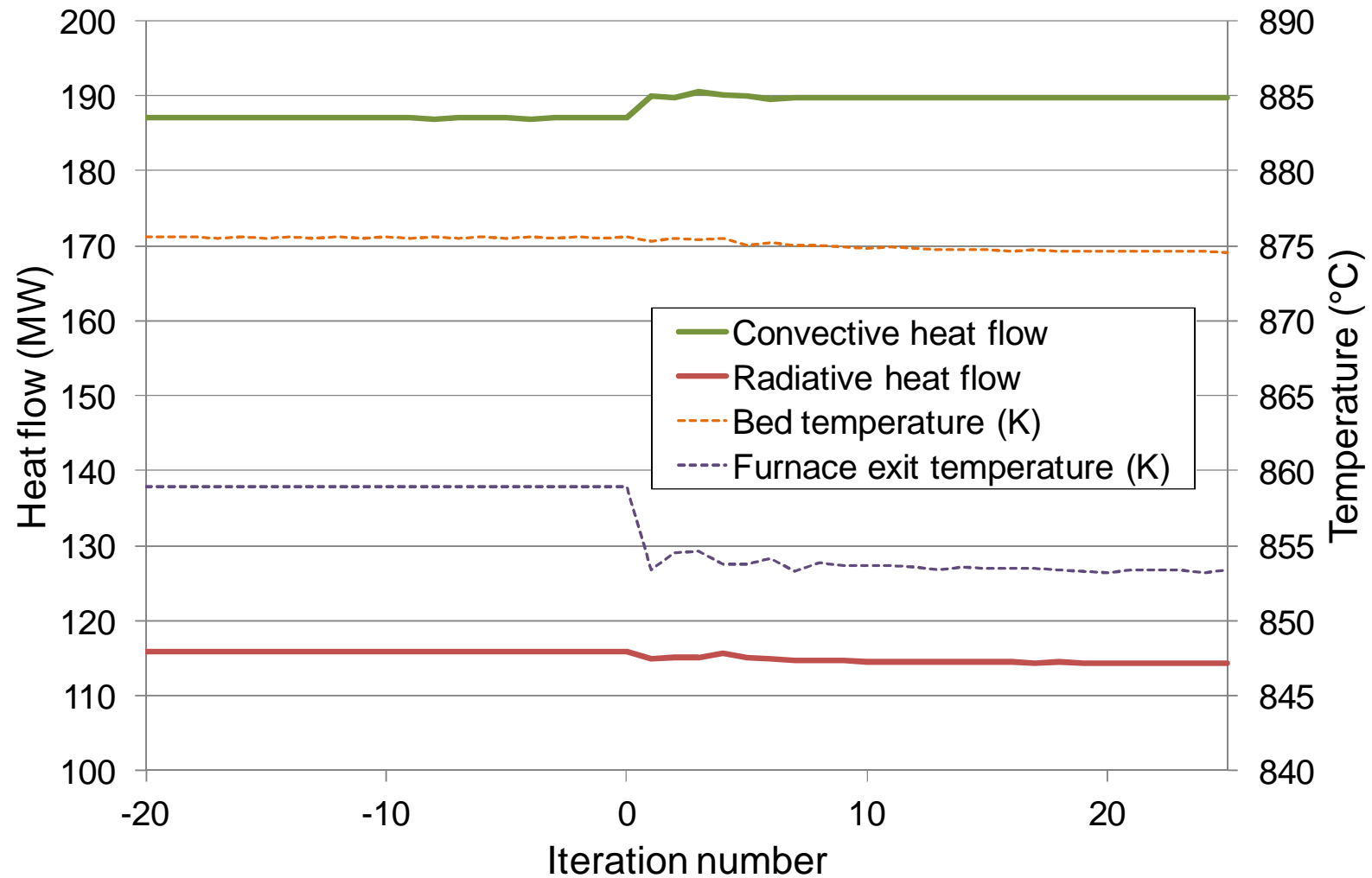
# Example of data exchange: radiative source



# Radiative source term for the inclined bottom part



# Development of total heat flows and average furnace temperatures

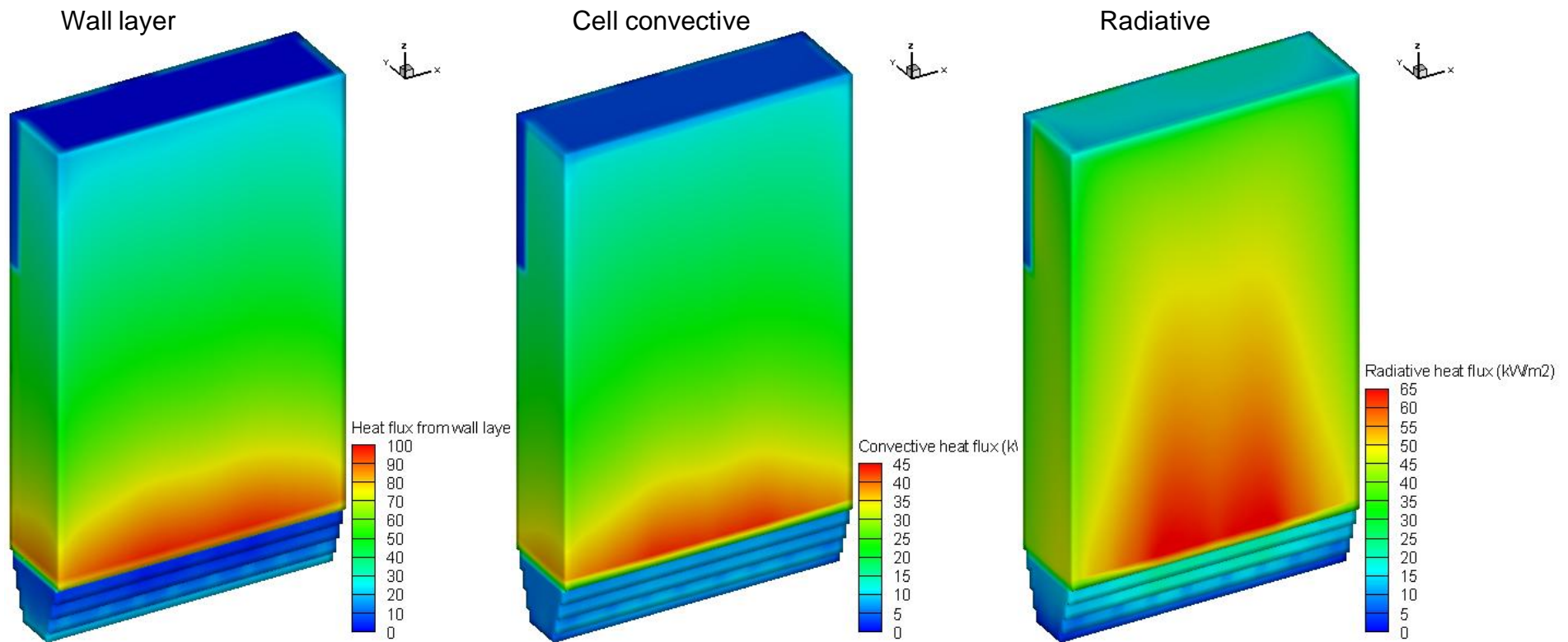


Iteration 0 is the converged solution without the radiation model.

# Heat flux modes without the radiation model

- Total heat flows by different modes (MW):

Wall layer	Cell convective	Radiative
127.6	59.3	115.8

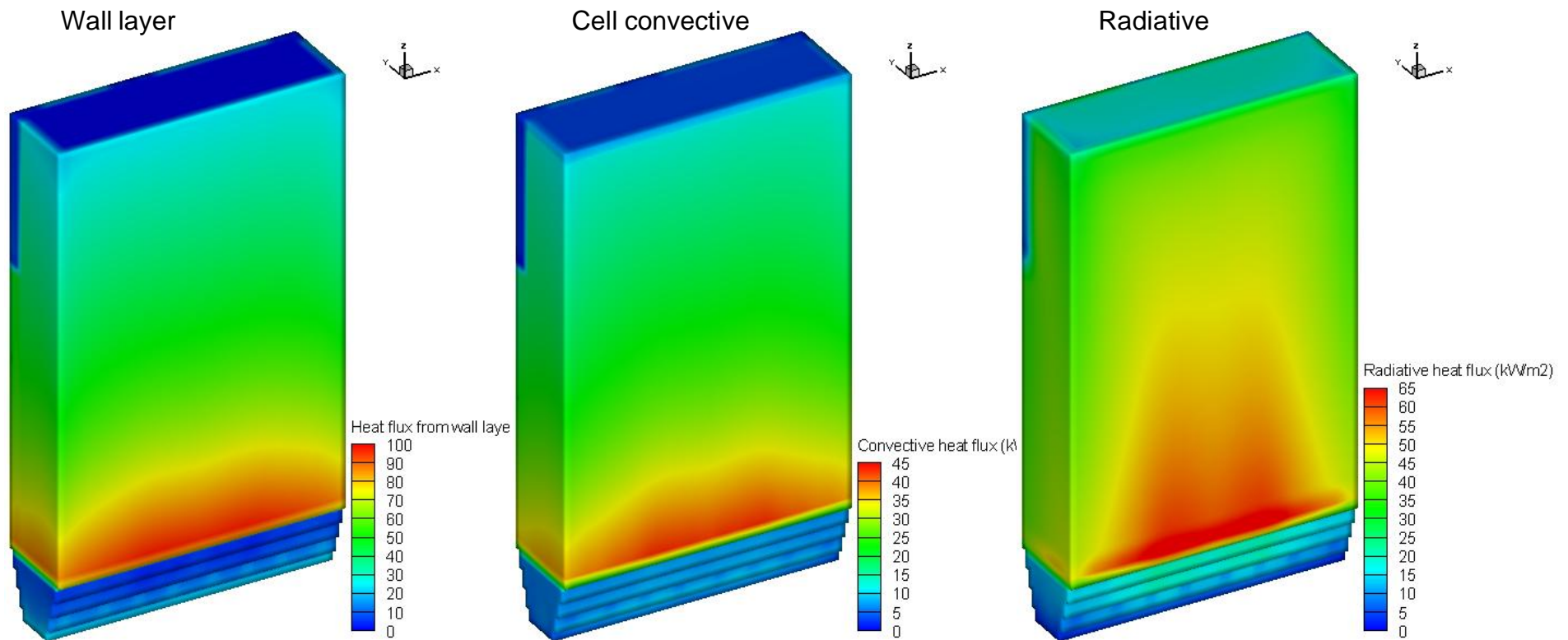


# Heat flux modes with the radiation model

- Total heat flows by different modes (kW):

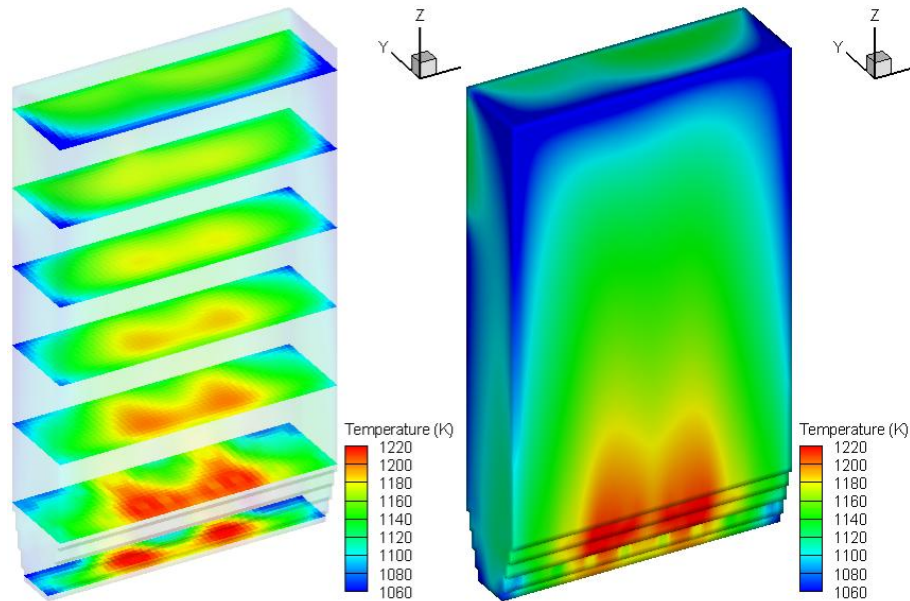
Wall layer	Cell convective	Radiative
130.0	59.7	114.3
+1.8%	+0.6%	-1.3%

(compared to results without radiation model)  
=> Slightly higher heat transfer in convective heat transfer modes

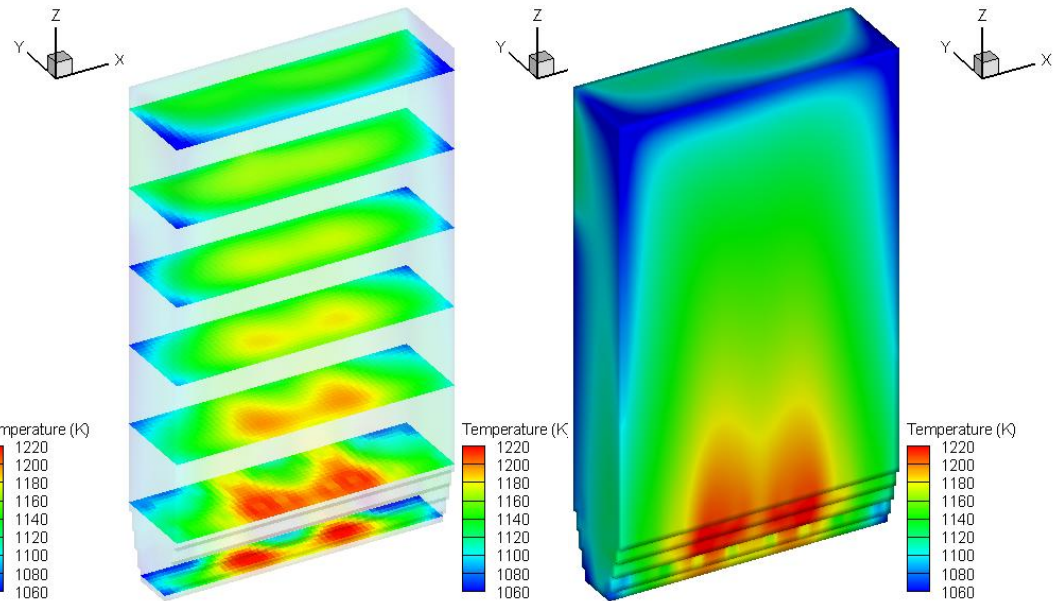


# Effect of radiation model on temperature field

Without radiation model



With radiation model



- With the radiation model, the temperature profiles are more uniform at the upper furnace.
- The temperature near the walls increases, which increases the convective heat transfer.
- All in all, the changes are relatively small in this case. The situation may change in small load calculations.

# Summary

- The radiative zone model and the 3D process model for circulating fluidized bed furnace were successfully integrated.
- The radiation model can be (and has been) combined with other solvers as well, e.g. with Fluent.
- With the radiation model, the temperatures inside the furnace were more uniform and the total heat flux to furnace walls was slightly increased.
  - In this case (100% load point), the changes were small.
- The radiation model will be further developed to overcome the current limitations.
- The modeling concept can be applied to study different process conditions, e.g. operation with small load.



# References

- Bordbar, M.H., Hyppänen, T. (2007). Modeling of radiation heat transfer in a boiler furnace. *Adv. Stud. in Theor. Phys.* 1, 571-584.
- Myöhänen, K., Hyppänen, T. (2011). A three-dimensional model frame for modelling combustion and gasification in circulating fluidized bed furnaces. *Int. J. of Chem. Reactor eng.*, 9, Article A25.